



COURSE OVERVIEW PE0263

Fired Heaters, Air Coolers, Heat Exchangers, Pumps, Compressors, Pressure Vessels & Valves

Course Title

Fired Heaters, Air Coolers, Heat Exchangers, Pumps, Compressors, Pressure Vessels & Valves

Course Date/Venue

January 21-25, 2024/The Paragon Meeting Room, The H Dubai Hotel, Sheikh Zayed Rd - Trade Centre, Dubai, UAE

Course Reference

PE0263



Course Duration/Credits

Five days/3.0 CEUs/30 PDHs

Course Description



This practical and highly-interactive course includes various practical sessions and exercises. Theory learnt will be applied using our state-of-the-art simulators.

This course is designed to provide delegates with a detailed and up-to-date overview of fired heaters, air coolers, heat exchangers, pumps, compressors, crude desalter, pressure vessels & valves operations. It covers the objective and equipment layout of process equipment; developing of static and dynamic head in the operating volume of pumps for efficiency and control operation; the affinity laws as tools for efficient operation, pump auxiliaries, wear components, canned motor and magnetic drive pumps, flow pumps, servicing and condition monitoring; the main features of various types of compressors; the compressors classification based on design and application; the types, styles and configurations of centrifugal and axial compressors; and the main elements of centrifugal compressor construction and efficiency.



During this interactive course, participants will learn the compressor operation; the fin fan cooler including its types, operational efficiency and capacity control; the operation and troubleshooting of cooler; the heaters and their types, construction and operating parameters and inspection/testing requirements; the types and basic parts of furnaces; the fuel gas system of burners, gas burners, oil burners, flame impingement, draft and observations during normal operation; the heat exchangers, process vessels and valves; and the troubleshooting of different equipment and processes.



Course Objectives

Upon the successful completion of this course, each participant will be able to:-

- Apply and gain an in-depth knowledge on fired heaters, air coolers, heat exchangers, pumps, compressors, crude desalter, pressure vessels & valves operations
- Discuss process equipment including its objective and equipment layout
- Develop static and dynamic head in the operating volume of pumps for efficiency and control operation
- Discuss the affinity laws as tools for efficient operation, pump auxiliaries, wear components, canned motor and magnetic drive pumps, flow pumps, servicing and condition monitoring
- Explain the main features of various types of compressors, classify compressors based on design and application including world standards and codes related to compressor
- Identify the types, styles and configurations of centrifugal compressors and axial compressors
- Explain the main elements of centrifugal compressor construction and analyze centrifugal compressor efficiency
- Employ guidelines for trouble-free centrifugal compressor operation including troubleshooting, inspection and maintenance
- Operate compressor by analysing curves for surge, stall and choke as well as define appropriate equipment for safe operation
- Recognize fin fan cooler including its types, operational efficiency and capacity control
- Operate and troubleshoot cooler through key operational considerations and proper troubleshooting
- Discuss heaters and their types, construction and operating parameters, inspection/testing requirements
- Identify the types and basic parts of furnaces including their efficient operation and air control
- Analyze the fuel gas system of burners, gas burners, oil burners, flame impingement, draft and observations during normal operation
- Differentiate heat exchangers, process vessels and valves
- Troubleshoot different equipment and processes in a professional manner

Exclusive Smart Training Kit - H-STK®



Participants of this course will receive the exclusive “Haward Smart Training Kit” (**H-STK®**). The **H-STK®** consists of a comprehensive set of technical content which includes **electronic version** of the course materials, sample video clips of the instructor’s actual lectures & practical sessions during the course conveniently saved in a **Tablet PC**.

Who Should Attend

This course provides an overview of an overview of all significant aspects and considerations of operation of process equipment for engineers, design engineers, maintenance staff and other technical staff.




Course Certificate(s)

Internationally recognized certificates will be issued to all participants of the course who completed a minimum of 80% of the total tuition hours.

Certificate Accreditations


Certificates are accredited by the following international accreditation organizations: -

-  The International Accreditors for Continuing Education and Training (IACET USA)

Haward Technology is an Authorized Training Provider by the International Accreditors for Continuing Education and Training (IACET), 2201 Cooperative Way, Suite 600, Herndon, VA 20171, USA. In obtaining this authority, Haward Technology has demonstrated that it complies with the **ANSI/IACET 2018-1 Standard** which is widely recognized as the standard of good practice internationally. As a result of our Authorized Provider membership status, Haward Technology is authorized to offer IACET CEUs for its programs that qualify under the **ANSI/IACET 2018-1 Standard**.

Haward Technology’s courses meet the professional certification and continuing education requirements for participants seeking **Continuing Education Units (CEUs)** in accordance with the rules & regulations of the International Accreditors for Continuing Education & Training (IACET). IACET is an international authority that evaluates programs according to strict, research-based criteria and guidelines. The CEU is an internationally accepted uniform unit of measurement in qualified courses of continuing education.

Haward Technology Middle East will award **3.0 CEUs** (Continuing Education Units) or **30 PDHs** (Professional Development Hours) for participants who completed the total tuition hours of this program. One CEU is equivalent to ten Professional Development Hours (PDHs) or ten contact hours of the participation in and completion of Haward Technology programs. A permanent record of a participant’s involvement and awarding of CEU will be maintained by Haward Technology. Haward Technology will provide a copy of the participant’s CEU and PDH Transcript of Records upon request.

-  British Accreditation Council (BAC)

Haward Technology is accredited by the **British Accreditation Council for Independent Further and Higher Education** as an **International Centre**. BAC is the British accrediting body responsible for setting standards within independent further and higher education sector in the UK and overseas. As a BAC-accredited international centre, Haward Technology meets all of the international higher education criteria and standards set by BAC.

Accommodation

Accommodation is not included in the course fees. However, any accommodation required can be arranged at the time of booking.

Course Fee

US\$ 5,500 per Delegate + **VAT**. This rate includes H-STK® (Haward Smart Training Kit), buffet lunch, coffee/tea on arrival, morning & afternoon of each day. In addition to the Course Manual, participants will receive an e-book “*Operator’s Guide to Rotating Equipment Construction, Operating Principles, Troubleshooting and Best Practices*”, published by AuthorHouse.





Course Instructor(s)

This course will be conducted by the following instructor(s). However, we have the right to change the course instructor(s) prior to the course date and inform participants accordingly:



Dr. Hesham Abdou, PhD, MSc, PgDip, BSc, is a Senior Process & Petroleum Engineer with 40 years of integrated experience within the Oil & Gas industries. His specialization widely covers in the areas of Artificial Lift System, Artificial Lift Methods, Petroleum Economics, Petroleum Refinery Processing, Refinery Material Balance Calculation, Refinery Gas Treating, Asset Operational Integrity, Drilling Operations, Drilling Rig, Bits & BHA, Mud Pumps, Mud logging Services, Wireline & LWD Sensors, Casing & Cementing Operation, Completion & Workover Operations, Petroleum Engineering, Production Optimization, Well Completion, Rig & Rigless Workover,

Advanced PVT & EOS Characterization, PVT/Fluid Characterization/EOS, Advanced Phase Behaviour & EOS Fluid Characterization, PVT Properties of Reservoir Fluids, Directional Drilling Fundamentals, Application & Limitation, Horizontal & Multilateral Wells (Analysis & Design), Directional, Horizontal & Multilateral Drilling, Root Cause Analysis (RCA), Root Cause Failure Analysis (RCFA), Root Cause Analysis Study, Root Cause Analysis Techniques & Methodologies, Process Hazard Analysis (PHA), Crude Oil Testing & Water Analysis, Crude Oil & Water Sampling Procedures, Equipment Handling Procedures, Crude & Vacuum Process Technology, Gas Conditioning & Processing, Cooling Towers Operation & Troubleshooting, Sucker Rod Pumping, ESP & Gas Lift, PCP & Jet Pump, Pigging Operations, Electric Submersible Pumps (ESP), Progressive Cavity Pumps (PCP), Natural & Artificial Flow Well Completion, Well Testing Procedures & Evaluation, Well Performance, Coiled Tubing Technology, Oil Recovery Methods Enhancement, Well Integrity Management, Well Casing & Cementing, Acid Gas Removal, Heavy Oil Production & Treatment Techniques, Water Flooding, Water Lift Pumps Troubleshooting, Water System Design & Installation, Water Networks Design Procedures, Water Pumping Process, Pipelines, Pumps, Turbines, Heat Exchangers, Separators, Heaters, Compressors, Storage Tanks, Valves Selection, Compressors, Tank & Tank Farms Operations & Performance, Oil & Gas Transportation, Oil & Gas Production Strategies, Artificial Lift Methods, Piping & Pumping Operations, Oil & Water Source Wells Restoration, Pump Performance Monitoring, Rotor Bearing Modelling, Hydraulic Repairs & Cylinders, Root Cause Analysis, Vibration & Condition Monitoring, Piping Stress Analysis, Amine Gas Sweetening & Sulfur Recovery, Heat & Mass Transfer and Fluid Mechanics.

During his career life, Dr. Hesham held significant positions and dedication as the **General Manager, Petroleum Engineering Assistant General Manager, Workover Assistant General Manager, Workover Department Manager, Artificial Section Head, Oil & Gas Production Engineer** from Agiba Petroleum Company and **Engineering Consultant/Instructor** for various Oil & Gas companies as well as a **Senior Instructor/Lecturer** for **PhD, Master & BSc degree students** from various universities such as the Cairo University, Helwan University, British University in Egypt, Banha University.

Dr. Hesham has **PhD** and **Master** degrees as well as **Post Graduate Diploma in Mechanical Power Engineering** and a **Bachelor** degree in **Petroleum Engineering**. Further, he is a **Certified Instructor/Trainer** and a **Peer Reviewer**. Dr. Hesham is an active member of Egyptian Engineering Syndicate and the Society of Petroleum Engineering. Moreover, he has published technical papers and journals and has delivered numerous trainings, workshops, courses, seminars and conferences internationally.



Training Methodology

All our Courses are including **Hands-on Practical Sessions** using equipment, State-of-the-Art Simulators, Drawings, Case Studies, Videos and Exercises. The courses include the following training methodologies as a percentage of the total tuition hours:-

- 30% Lectures
- 20% Practical Workshops & Work Presentations
- 30% Hands-on Practical Exercises & Case Studies
- 20% Simulators (Hardware & Software) & Videos

In an unlikely event, the course instructor may modify the above training methodology before or during the course for technical reasons.

Course Program

The following program is planned for this course. However, the course instructor(s) may modify this program before or during the course for technical reasons with no prior notice to participants. Nevertheless, the course objectives will always be met:

Day 1: Sunday, 21st of January 2024

0730 – 0800	Registration & Coffee
0800 – 0815	Welcome & Introduction
0815 – 0830	PRE-TEST
0830 – 0930	Introduction to Process Equipment Process Equipment Objective • Types of Process Plants • Process Equipment Layout • Rotating Equipment • Stationery Equipment
0930 – 0945	Break
0945 – 1100	Pumps Development of Static and Dynamic Head in the Operating Volume of Pumps for Efficiency and Control Operation • The Affinity Laws as Tools for Efficient Operation • Pump Auxiliaries
1100 – 1230	Pumps (cont'd) Wear Components • Canned Motor and Magnetic Drive Pumps • High Speed/Low Flow Pumps • Servicing and Condition Monitoring
1230 – 1245	Break
1245 – 1420	Compressor Overview Overview of the Main Features of Various Types of Compressors • Classification of Compressors Based on Design and Application • World Standards and Codes Related to Compressor Design
1420 – 1430	Recap
1430	Lunch & End of Day One

Day 2: Monday, 22nd of January 2024

0730 – 0930	Types of Compressors Types, Styles and Configurations of Centrifugal and Axial Compressors • Construction Features • Mode of Operation • Compressor Auxiliaries and Support Systems
0930 – 0945	Break
0945 – 1100	Centrifugal Compressor Main Elements of Centrifugal Compressor Construction • Analysis of Centrifugal Compressor Efficiency • Guidelines for Trouble-free Centrifugal Compressor Operation





1100 – 1230	Centrifugal Compressor (cont'd) Troubleshooting Inspection and Maintenance • Centrifugal Compressors Anti Surge System and Surge Protection • Case Studies About Centrifugal Compressors
1230 – 1245	Break
1245 – 1420	Compressor Operation Analyse Operating Curves for Surge, Stall and Choke • Define Appropriate Equipment for Safe Operation
1420 – 1430	Recap
1430	Lunch & End of Day Two

Day 3: Tuesday, 23rd of January 2024

0730 – 0930	Fin Fan Cooler Types • Operational Efficiency • Capacity Control
0930 – 0945	Break
0945 – 1100	Cooler Operating & Troubleshooting Key Operational Considerations • Air vs Water Cooling • Troubleshooting
1100 – 1230	Heater Heaters and their Types • Construction & Operating Parameters • Inspection/Testing Requirements
1230 – 1245	Break
1245 – 1420	Furnaces Types of Furnaces • Furnace Basic Parts • Efficient Operation, Air Control etc
1420 – 1430	Recap
1430	Lunch & End of Day Three

Day 4: Wednesday, 24th of January 2024

0730 – 0930	Fuel Gas System Burners • Gas Burners • Oil Burners
0930 – 0945	Break
0945 – 1100	Fuel Gas System (cont'd) Flame Impingement • Draft • Observations During Normal Operation
1100 – 1230	Heat Exchangers Types • Shell-and-Tube
1230 – 1245	Break
1245 – 1420	Heat Exchangers (cont'd) Heat Transfer Relation
1420 – 1430	Recap
1430	Lunch & End of Day Four

Day 5: Thursday, 25th of January 2024

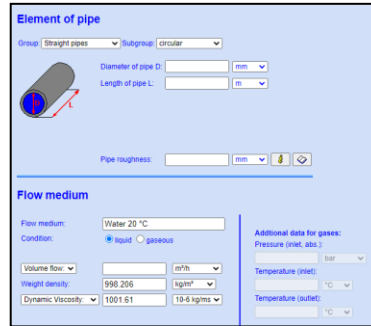
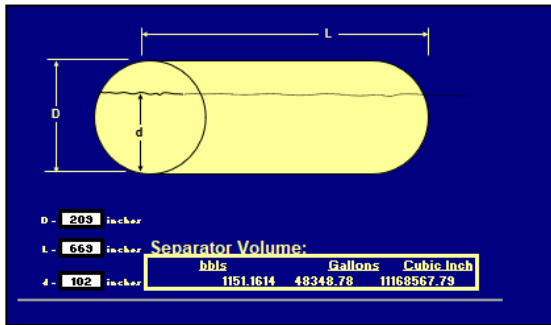
0730 – 0930	Process Vessels Types and Functions • Safety Aspects
0930 – 0945	Break
0945 – 1215	Valves Valve Theory • Valve Types • Applications
1215 – 1230	Break
1230 – 1245	Valves (cont'd) Function • Operation • Troubleshooting
1245 – 1345	Troubleshooting of Different Equipment & Processes
1345 – 1400	Course Conclusion
1400 – 1415	POST-TEST
1415 – 1430	Presentation of Course Certificates
1430	Lunch & End of Course





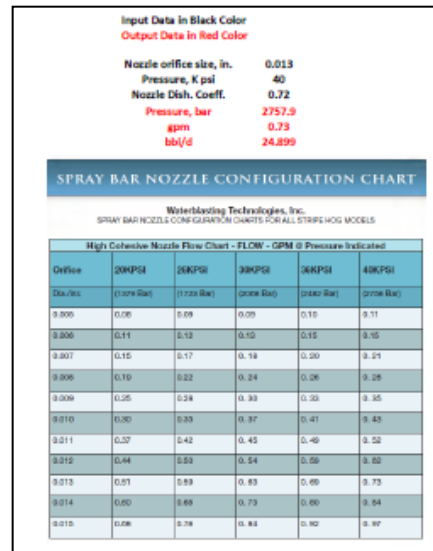
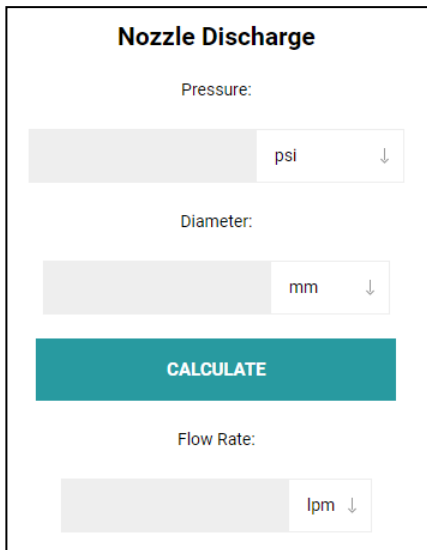
Simulator (Hands-on Practical Sessions)

Practical sessions will be organized during the course for delegates to practice the theory learnt. Delegates will be provided with an opportunity to carryout various exercises using various online system calculator.



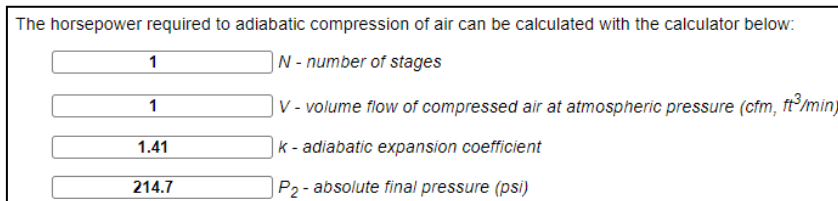
Tank Volume Calculator

Pressure Drop Online-Calculator



Nozzle Discharge

Nozzle Calculator



Horsepower Calculator



Water Flow Rate through an Orifice Calculator



Convert Cubic Feet Of Natural Gas to Barrels Of Oil Equivalent

Cubic Feet Of Natural Gas

Barrels Of Oil Equivalent (bboe)

Cubic Feet Calculator

Corrosion Rate Calculator

Enter data in given fields and click on Calculate for resultant corrosion rate.

Weight Loss **microgm** **Density** **gm/cm3**

Area **mm2** **Time** **millisec**

Calculate

Result: Corrosion Rate in **mpy**

Corrosion Rate Calculator

HYDRONICS CALCULATOR

Water velocity calculator

Water Flow Rate (gpm) gpm

Pipe diameter (DN/IN) DN/IN

V = ft/min

Calculate **Reset**

Minimum pipe diameter calculator

Water Flow Rate (gpm) gpm

Water Velocity (ft/min) ft/min

D = DN/IN

Calculate **Reset**

Water flow rate calculator

Pipe Diameter (DN/IN) DN/IN

Water Velocity (ft/min) ft/min

Q = gpm

Calculate **Reset**

Flow Rate (GPM)	Velocity (ft/min)	Pressure Drop (psi/100ft)
1	1.08	0.0001
2	2.16	0.0004
3	3.24	0.0009
4	4.32	0.0016
5	5.40	0.0025
6	6.48	0.0036
7	7.56	0.0049
8	8.64	0.0064
9	9.72	0.0081
10	10.80	0.0100
12	12.96	0.0144
15	16.20	0.0225
20	21.60	0.0360
25	27.00	0.0525
30	32.40	0.0720
40	43.20	0.1200
50	54.00	0.1800
60	64.80	0.2500
70	75.60	0.3200
80	86.40	0.4000
90	97.20	0.4900
100	108.00	0.5800

Hydronics Calculator

Pipe Pressure Loss Calculator

Inputs

Pressure at A (absolute): **kPa**

Average fluid velocity in pipe, V: **m/s**

Pipe diameter, D: **cm**

Pipe relative roughness, e/D: **m/m**

Pipe length from A to B, L: **m**

Elevation gain from A to B, z2: **m**

Fluid density, ρ: **kg/l**

Fluid viscosity (dynamic), μ: **cP**

Pipe Pressure Loss Calculator

BTU-Calculator-&-BTU-Formulas-for-Water-Circulating-Heat-Transfer

Weighed Water Test

Measure the flow of water through your process by timing how long it takes to fill a known volume container. For example, allow your process water to fill a 5-gallon container. Accurately measure the water temperature entering and exiting your process. Use this formula to calculate BTU cooling required:

Formula

BTU = Flow Rate In GPM (of water) x (Temperature Leaving Process - Temperature Entering Process) x 500.4*Formula changes with fluids others than straight water.

BTU Calculator for Weighed Water Test

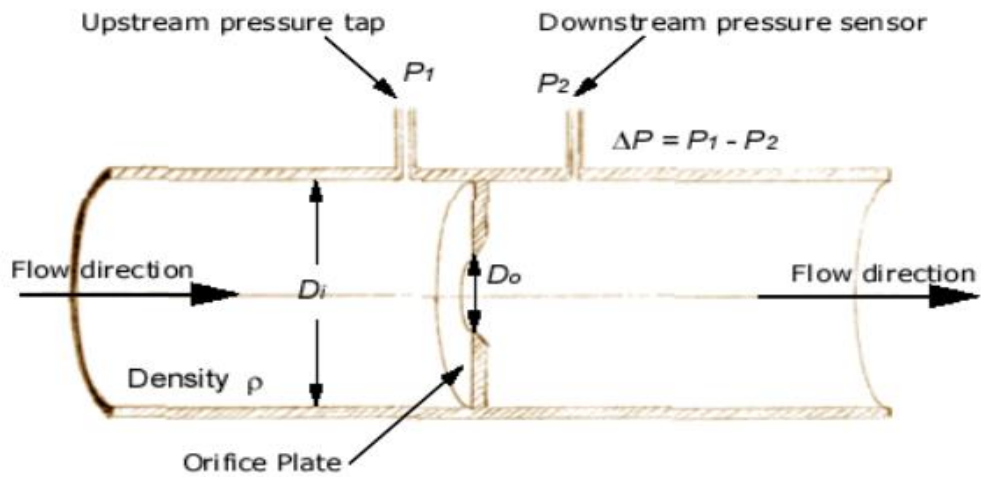
Water Flow Rate In Gallons Per Minute **GPM**

Inlet Water Temperature To Process **°F**

Outlet Water Temperature From Process **°F**

BTU Calculator





Inputs

Pipe (inlet) diameter upstream of orifice, D_i :	8	in ▾
Orifice diameter (less than the inlet diameter), D_o :	3	in ▾
Pressure difference across the orifice, Δp :	20	psi ▾
Fluid density, ρ :	835	kg/m ³ ▾
Flow Coefficient, C_f :	0.82	

Answers

Velocity at the inlet, V_i :	2.10 m/s	m/s ▾
Volumetric Flowrate, Q :	1080 gpm	gpm ▾
Mass Flowrate:	56.7 kg/s	kg/s ▾

Flow Rate through an Orifice or Valve Calculator



Net Positive Suction Head Calculator - In terms of head

Pump Formulas Calculator — Imperial and SI Units

Select a System Units
 Imperial Units SI Units

Ha
Imperial Units Ha = absolute pressure of the suction vessel, ft // SI Units Ha = absolute pressure of the suction vessel, m

Hvpa
Imperial Units fluid vapor pressure at pumping temperature, R // SI Units Hvpa = fluid vapor pressure at pumping temperature, m

Hst
Imperial Units Hst = static head to suction reference point (usually center line of the impeller), ft // SI Units Hst = static head to suction reference line (usually center point of the impeller), m

Hfs
Imperial Units Hfs = suction line losses, ft // SI Units Hfs = suction line losses, m

NPSH = net positive suction head at reference point usually center line of the impeller,
 ft
Imperial Units NPSH = net positive suction head at reference point (usually center line of the impeller), ft // SI Units NPSH = net positive suction head at reference point (usually center line of the impeller), m

Net Positive Suction Head Calculator

Net Positive Suction Head Calculator - In terms of pressure and head

Pump Formulas Calculator — Imperial and SI Units

Select a System Units
 Imperial Units SI Units

Pa
Imperial Units Pa = absolute pressure of the suction vessel, psia // SI Units Pa = absolute pressure of the suction vessel, kPa

Pvpa
Imperial Units Pvpa = fluid vapor pressure at pumping temperature, psia // SI Units Pvpa = fluid vapor pressure at pumping temperature, kPa absolute

Hst
Imperial Units Hst = static head to suction reference point (usually center line of the impeller), ft // SI Units Hst = static head to suction reference line (usually center point of the impeller), m

Hfs
Imperial Units Hfs = suction line losses, ft // SI Units Hfs = suction line losses, m

SG
SG = specific gravity

NPSH = net positive suction head at reference point usually center line of the impeller,
 ft
Imperial Units NPSH = net positive suction head at reference point (usually center line of the impeller), ft // SI Units NPSH = net positive suction head at reference point (usually center line of the impeller), m

Net Positive Suction Head Calculator

Input Data in Black Color
 Output Data in Red Color

lbs/gall. 11
 kg/lit. 1.318

Pounds per Gallon	Kilograms per Liter	Conversion Factor
7.0 lb/gal	0.84 kg/l	0.92
8.0 lb/gal	0.96 kg/l	0.98
8.34 lb/gal	1.00 kg/l (water)	1.00
9.0 lb/gal	1.08 kg/l	1.04
10.0 lb/gal	1.20 kg/l	1.10
10.65 lb/gal	1.28 kg/l (28% Nitrogen)	1.13
11.0 lb/gal	1.32 kg/l	1.15
12.0 lb/gal	1.44 kg/l	1.20
14.0 lb/gal	1.68 kg/l	1.30

PPG to KG Calculator

Liquid Pipeline Calculator Software

Inputs

Pressure at A (absolute): 1000 psi

Average fluid velocity in pipe, V: 5.1674 ft/s

Pipe diameter, D: 14 in

Pipe relative roughness, e/D: 0.000357 in/in

Pipe length from A to B, L: 80 km

Elevation gain from A to B, Δz: 0 ft

Fluid density, ρ: 965.44 kg/m³

Fluid viscosity (dynamic), μ: 5 cP

Liquid Pipeline Calculator

Cv Calculator for Valve Sizing

Calculation type
 Cv Flow

Medium Type
 Liquid Gas

Inlet pressure (P1): [] PSIA

Outlet pressure (P2): [] PSIA

Flow rate (Q): [] SCFM

Temperature: [] °Fahrenheit

System medium: Acetylene

Specific gravity: 0.907

CALCULATE

Cv Calculator

Find Flow

$$Q = C_d A \sqrt{\frac{2}{\rho} \Delta P}$$

Coefficient: 0.62

Specific Gravity: 0.875

Diameter: [] mm

Pressure Drop: [] bar

Flow: [] lpm

Find Flow Calculator

Inputs

Pipe (inlet) diameter upstream of orifice, D_i: 10 cm

Orifice diameter (less than the inlet diameter), D_o: 8 cm

Pressure difference across the orifice, Δp: 10 Pa

Fluid density, ρ: 1.29 kg/m³

Flow Coefficient, C_v: 0.7

Flowrate Calculator



Coefficient-of-Discharge-Calculator

Calculate discharge coefficient...

using... [hydraulic head](#)

Water level

H

d

Q

Flow parameters

Diameter (d) [m](#)

Area (A) [m²](#)

Head (H) [m](#)

Actual discharge (Q) [m³/s](#)

Coefficient Discharge Calculator

Convert horsepower hour to gallon [U.S.] of diesel oil

horsepower hour

gallon [U.S.] of diesel oil

[Convert](#)

Horsepower Hour Calculator



Liquid Pumping Program

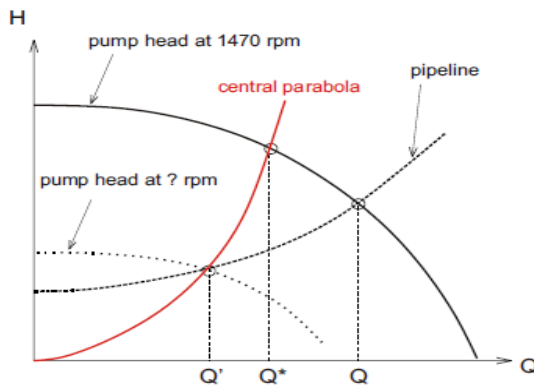
Input Data	
API	28
c.P.	5
1000 bbl/d	3.3
Length, km	2.4384
I.D., in.	2.800
Rough. (E), in.	0.005
Difference in elev., m	50
Destination press., psi	60
Pump Suc. psi	80
Overall Pump Eff., %	65
Motor Eff., %	90
Motor Loading %	80

Output Results

Flow Velocity, ft/s	5.0154
Erosion Velocity, ft/s	13.440
E/I.D.	0.001786
sp.gr.	0.8871
Re	19290.3
F	0.02987
Hf, psi	153.67
Hf, m water	108.17
Total Pump Dich. psi	276.68
TDP, psi	196.68
Hydr. Power, HP	16.99
Hydr. Power, Kw	12.67
Shaft Power, HP	18.88
Shaft Power, Kw	14.083
Nama Plate Motor HP	23.60
Nama Plate Motor Kw	17.60

A pump running at 1470[rpm] with $H_{pump} = 45 - 2781Q^2$ head delivers water into a pipeline with $H_{pipe} = 20 + 1125Q^2$. Calculate the required revolution number for the reduced flow rate $Q' = 0.05[m^3/s]$.

Solution:



- The actual working point is given by the solution of $H_{pump} = H_{pipe}$, which gives $Q = 0.08[m^3/s]$ and $H = 27.2[m]$.
- Affinity states that while varying the revolutionary speed, H/n^2 and Q/n remain constant. Thus, also H/Q^2 remains constant, let's denote this constant by a . So, while varying the revolutionary speed, the working point moves along the *central parabola* (see figure), given by $H_{ap} = aQ^2$.

However, as Q' is given and we also know that this point has to be located on the pipeline characteristic, we know that $H' = 20 + 1125 \times 0.05^2 = 22.81[m]$. Thus, the parameter of the affine parabola is $a = H'/Q'^2 = 9125$.

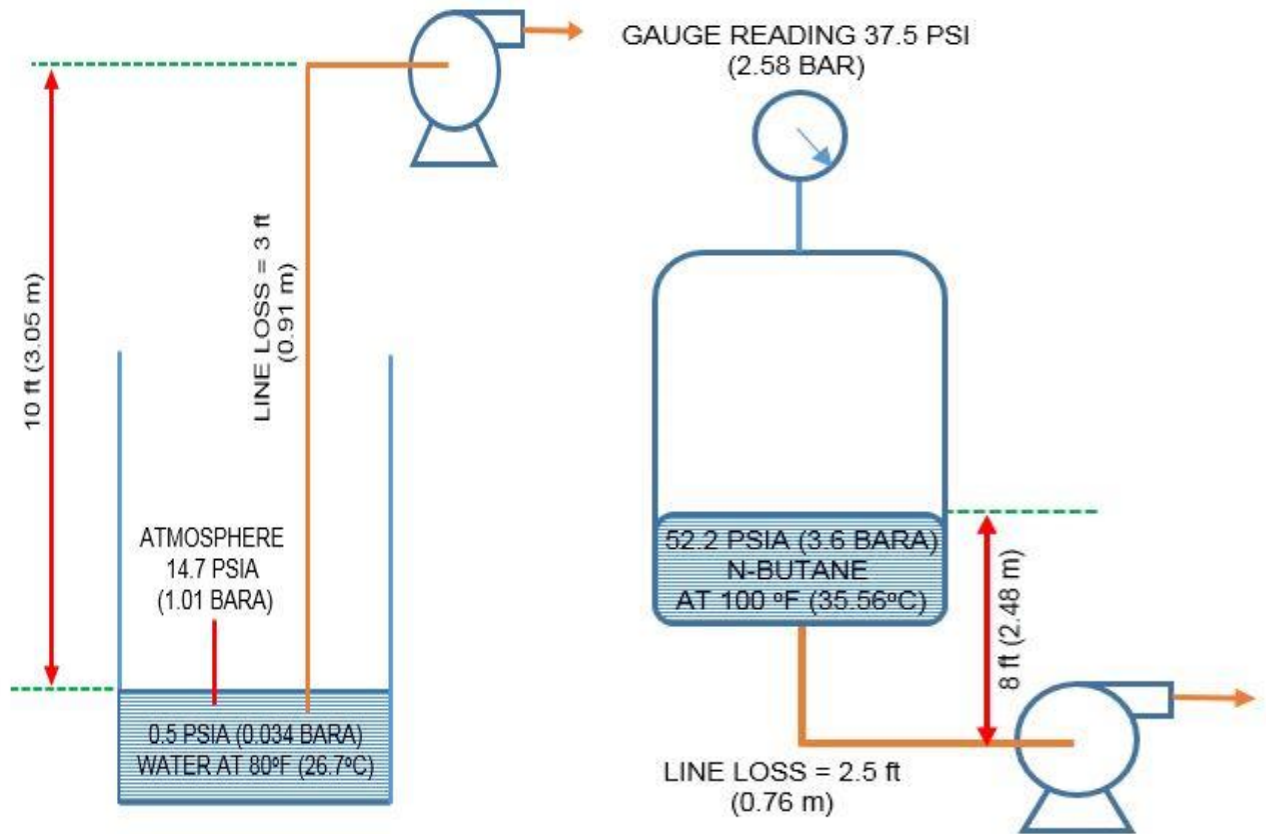
Q^* is given by the intersection of the affine parabola and the original pump characteristic: $H_{ap}(Q^*) = H_{pump}(Q^*)$, which gives $Q^* = 0.06148[m^3/s]$ with $H^* = 34.5[m]$.

Now we can employ affinity between Q^* and Q' :

$$n' = n^* \frac{Q'}{Q^*} = 1470 \times \frac{0.05}{0.06148} = 1195.5[rpm]$$

and just for checking the calculation

$$H' = H^* \left(\frac{n'}{n^*} \right)^2 = 34.5 \times \frac{1195.5^2}{1470^2} = 22.81[m].$$



NPSHA of pump – suction lift

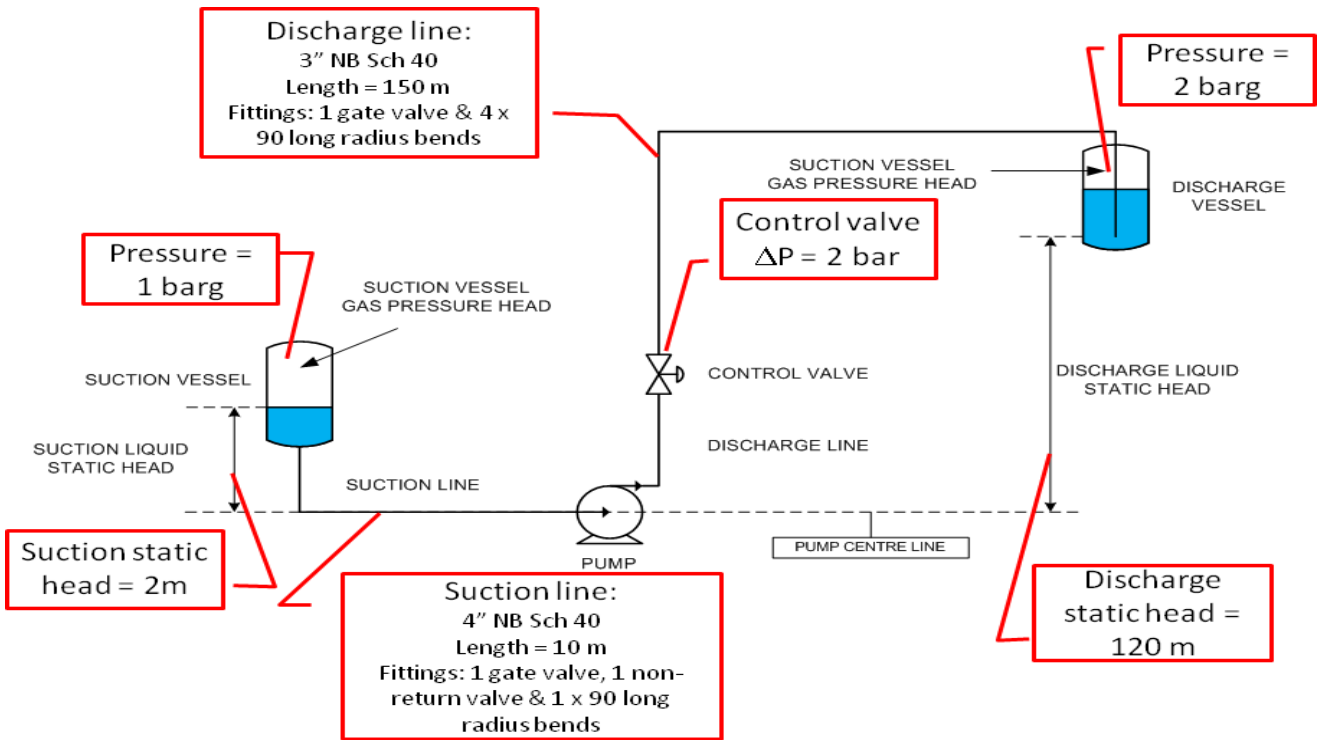
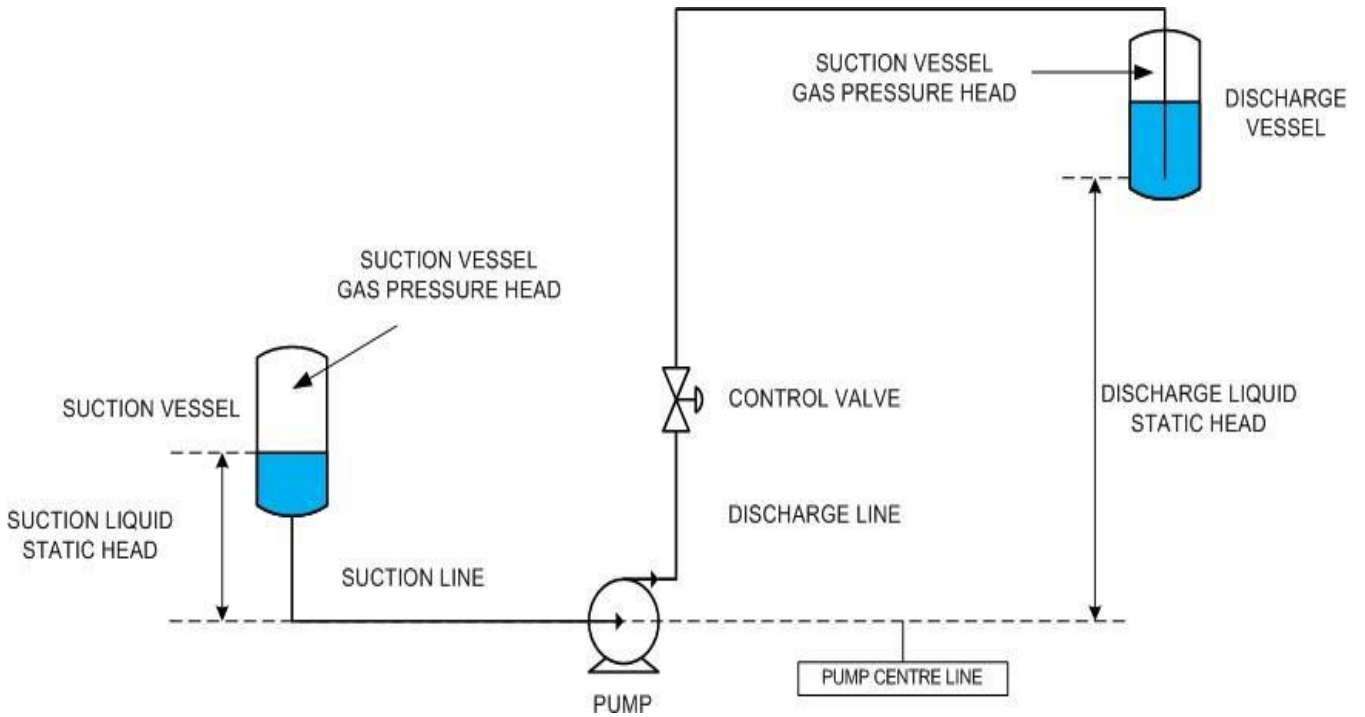
NPSHA of pump – at boiling point
SG of n-butane at 100 deg F = 0.56

$$NPSHA = Hatmp. +/- Hs - Hf - Hvap.$$

https://engineeringunits.com/net-positive-suction-head-calculator/?utm_content=cmp-true

<http://www.pressure-drop.com/Online-Calculator/index.html>

NPSH Calculations		Output Results	
Input Data		Flow Velocity, ft/s	2.6620
API	36	E/I.D.	0.001671
c.P.	3	sp.gr.	0.8448
Vapor pressure, psi	10	Re	17363.9
Atmp. Pressure, psi	14.7	F	0.0302
Height above pump, ft	20	Hf, psi	0.048
1000 bbl/d	2.0	Hf, ft water	0.111
Length, km	0.003	NPSHA, ft oil	32.72
I.D., in.	2.992	NPSHA, ft water	27.64
Rough. (E), in.	0.005		





Calculator

PUMP DETAILS

Pump tag number		P-001
Suction vessel tag number		V-001
Discharge vessel tag number		V-002
Barometric pressure	P_{atm}	1.013 bara
NPSH available margin	H_{margin}	0 m
Pump efficiency	η	70%

FLUID PROPERTIES

Fluid		Water
Phase		Liquid
Flowrate	m	30000 kg/hr
Density	ρ	998 kg/m ³
Viscosity	μ	1 cP
Vapour pressure	P_{vap}	0.023 bara

VESSEL GAS PRESSURES

Suction vessel gas pressure	P_{suc_vessel}	1 barg
Discharge vessel gas pressure	P_{dis_vessel}	2 barg

STATIC HEADS

Suction static head	$H_{suc_static_head}$	2 m
Discharge static head	$H_{dis_static_head}$	120 m

PIPELINES

		Suction Line	Discharge Line	
Pipe nominal diameter		4	3	inch
Pipe schedule		Sch 40	Sch 40	
Pipe internal diameter	d	102.26	77.92	mm
Pipe length	L	10	150	m
Absolute roughness	e	0.046	0.046	mm

OUTPUTS

Volumetric flow rate Q 30.060 m³/hr

		Suction Line	Discharge Line	
Relative roughness	e:d	0.00045	0.00059	
Flow area	A	0.00821	0.00477	m ²
Velocity	u	1.02	1.75	m/s
Reynolds No.	Re	103758	136170	
Flow regime		turbulent	turbulent	
Friction factor	f	0.02011	0.02010	
Pipe velocity head loss	K_{pipe}	1.966	38.695	
Fittings total velocity head loss	$K_{fittings}$	1.724	2.152	
Frictional pressure loss	$\Delta P_{friction}$	0.02	0.62	bar
Frictional head loss	$H_{friction}$	0.19	6.38	m

Pump suction pressure	$P_{suction}$	2.19 bara
Pump suction head	$H_{suction}$	22.37 m
Pump discharge pressure	$P_{discharge}$	15.39 bara
Pump discharge head	$H_{discharge}$	157.16 m
Net positive suction pressure available	P_{NPSHA}	2.17 bara
Net positive suction head available	NPSHa	22.13 m
Pump total differential pressure	ΔP_{pump}	13.20 bar
Pump total differential head	H_{pump}	134.79 m
Pump absorbed power	E	15.74 kW





Results of above calculations may be confirmed through either of following links:

<https://www.swagelok.com/en/toolbox/cv-calculator>

https://experttoolsonline.com/danfoss/orifice_calculator

https://www.efunda.com/formulae/fluids/calc_orifice_flowmeter.cfm

<https://www.omnicalculator.com/physics/coefficient-of-discharge>

Power Calculations:

<https://inventory.powerzone.com/resources/centrifugal-pump-power-calculator/%3Aflu%3DGPM%3Apru%3DHEAD%20FT%3Apu%3DHP>

<http://irrigation.wsu.edu/Content/Calculators/General/Required-Water-Pump-HP.php>

Required Compressor Horsepower

https://www.engineeringtoolbox.com/horsepower-compressed-air-d_1363.html

<u>Input Data</u>		<u>Output Results</u>	
T1, F	60	Compression Ratio	34.014
K	1.35	Cp, J/kg/K	1107
P1, psi	14.7	Gas, cfm	36791.50
P2, psi	500	Gas, kg/s	21.250
Gas sp.gr.	1	Theoretical Power, HP	9731.847
No. of Comp. stages	3	Total Required HP	12721.37
Gas million SCMD	1.5		
Eff. of Gas Comp., %	85		
Eff. of Driving Motor, %	90		

Heater Duty

<https://www.advantageengineering.com/fyi/288/advantageFYI288.php>

<u>Input Data</u>		<u>Output Results</u>	
Million BTU/hr.	0.75	Delta Temp., C	15.6
API	10.0	Mega Watt	0.220
Specific Heat, BTU/lb/F	1.00	Billion Joule/hr.	0.791
Delta Temp., F	60	gpm	25.0
Heater Eff., %	100	gallon/hr.	1498.4
		Lit./min.	94.5
		m3/hr.	5.7
		1000 bbl/d	0.856
		Required Diesel Lit./day	502.90
		Required Diesel bbl/d	3.16
		Required Gas, 1000 ft3/d	16.364
		Required crude oil, bbl/d	3.268

<https://www.enggcyclopedia.com/2011/09/problem-solving-heat-exchanger-tubewise-pressure-drop-calculation/>





<u>Input Data</u>		<u>Output Results</u>	
Mass Flow Rate, kg/hr.	2000.0	cm ³ /s	562.303
Fluid Density, Kg/m ³	988.0	V, cm/s	110.9720
Visc., c.P.	0.53	Re	52544.59
Pipe Diameter (D), in.	1	f	0.0261
Roughness (E), mm	0.045	Total Hf, cm (per single tube)	22.5583
Tube Length, m	3.5	Total Hf, psi (per single tube)	0.3166
No. of tubes	1	Total Hf, bar (per single tube)	0.0218

Heat exchanger tube side pressure drop calculation

Calculate the tube side pressure drop for the following heat exchanger specification,

Process fluid = water

Inlet pressure = 4 barg

Inlet temperature = 50⁰C

Outlet temperature = 30⁰C

Tubeside flowrate = 50000 kg/hr

Number of tubes = 25

Tube ID (internal diameter) = 1 inch

Tube length = 3.5 m

Total volumetric flow = 50000 kg/hr ÷ 988.0 kg/m³ = 50.61 m³/hr Volumetric flow in each 1" tube = 50.61 ÷ 25 = 2.02 m³/hr Pressure loss per unit length of the tube is then calculated using [EnggCyclopedia's pressure drop calculators for pipes and tubes](#). This calculator is based on [Darcy-Weisbach equation](#).

Pressure loss across a single tube (ΔP/L) = 6.17 bar/km

SINGLE PHASEFLOW INPUTS

W – Mass flow capacity kg/h
 ρ – Density of fluid kg/m³
 μ – Viscosity of fluid (either liquid or gas) cP

PIPE SPECIFICATIONS

e – Effective roughness of the pipe mm
 d – Nominal diameter of the pipe inches
 sch – pipe schedule

RESULTS

Fluid Velocity m/s
 Volumetric flow m³/hr
Reynold's No.
Pressure loss bar/km

Tube length (L) = 3.5 m

Tubeside pressure drop (ΔP) = 6.17 × 3.5 / 1000 = 0.0216 bar





Another alternative is to directly use EnggCyclopedia's Heat Exchanger Tube side Pressure Drop Calculator. All the inputs given in the sample problem statements are given to the calculator and pressure drop across the tubeside is calculated as output. This calculator uses the same basic steps discussed above and hence the answer also matches with the figure above (0.0216 bar) . The following image is a snapshot of this direct calculation of tubeside pressure drop.

Exchanger tubeside pressure drop

Tubeside inputs

Total tubeside <u>mass</u> flow	50000	kg/hr
Tubeside <u>Density</u>	988	kg/m ³
Tubeside <u>Viscosity</u>	0.53	cP
Number of tubes	25	
Total tube length (accounting for all tube passes)	3.5	m
Tube nominal diameter	1	inches
Tubeside roughness	0.045	mm
<input type="button" value="Calculate pressure drop"/>	<input type="button" value="Reset"/>	

Results

Tubeside pressure drop	0.0216	bar
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Book(s)

As part of the course kit, the following e-book will be given to all participants:

<p>OPERATOR'S GUIDE to Rotating Equipment</p> <p>An introduction to rotating equipment construction, operating principles, troubleshooting, and best practices</p> <p>Julien LeBleu, Jr. and Robert Perez</p>	<p>Title : Operator's Guide to Rotating Equipment: An Introduction to Rotating Equipment Construction, Operating Principles, Troubleshooting and Best Practices</p> <p>ISBN : 978-1-49690-868-1</p> <p>Authors : Julien LeBleu Robert Perez</p> <p>Publisher : AuthorHouse</p>
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Course Coordinator

Kamel Ghanem, Tel: +971 2 30 91 714, Email: kamel@haward.org

